

**Mid-term Test**  
**SOLID MECHANICS (NASM)**  
**October 1, 2024, 11:00-11:45 h**

NB This is a *closed-book* exam. It comprises four problems, for which one can obtain the following points:

Question	# points
1	2
2	3
3	2
4	1+1=2

The number of points is indicated next to each subquestion inside a rectangular box in the right-hand margin on the next pages.

The mid-term grade is calculated as  $9 * (\# \text{ points}) / 9 + 1$  and contributes 30% to the final grade.

**Question 1** Prove that the outcome of the quadratic product  $\mathbf{x} \cdot \mathbf{A} \cdot \mathbf{x}$  for an arbitrary vector  $\mathbf{x}$  is independent of the skew-symmetric part of the tensor  $\mathbf{A}$ . 2

**Question 2** In two dimensions, let the components of the deformation gradient tensor be specified by the matrix

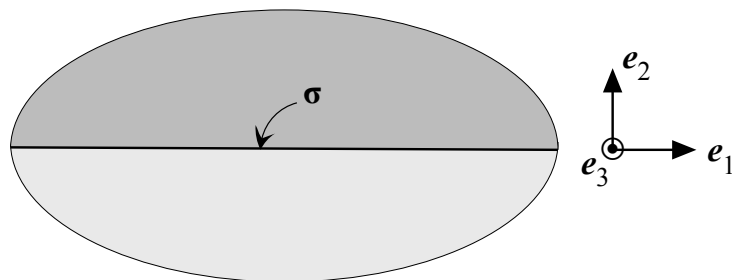
$$[F_{ij}] = \begin{bmatrix} 1 & 0 \\ \gamma & 1 \end{bmatrix}.$$

a. Show that the corresponding components of the strain tensor in the geometrically linear theory are given by 1

$$[\varepsilon_{ij}] = \begin{bmatrix} 0 & \gamma/2 \\ \gamma/2 & 0 \end{bmatrix}.$$

b. Is the inverse also correct? In other words: given these strain components, does this imply that the deformation gradient is as specified above? Explain your answer. 2

**Question 3** Consider a flat interface between two dissimilar materials in a loaded composite material. When the system is in equilibrium, which components of the stress tensor  $\boldsymbol{\sigma}$  in three dimensions are continuous across this interface (with unit normal  $\mathbf{n} = \mathbf{e}_2$ )? 2



**Question 4** Consider a planar strain state characterized by principal strains  $\varepsilon_1$  and  $\varepsilon_2$  with respect to the basis  $\{\mathbf{e}_1, \mathbf{e}_2\}$ ; that is,

$$[\varepsilon_{ij}] = \begin{bmatrix} \varepsilon_1 & 0 \\ 0 & \varepsilon_2 \end{bmatrix}.$$

When viewed from the vantage point of a basis  $\{\mathbf{e}_a^*\}$  ( $a = 1, 2$ ) that is rotated over an angle  $\theta$  in the plane, the strain components  $\varepsilon_{ab}^*$  will no longer be principal strains and shear strain components will emerge.

a. At what value of  $\theta$  will the shear strain component  $\varepsilon_{12}^*$  be maximal? 1

b. What is the normal strain component at this particular orientation? 1

**Solutions Mid-term Test**  
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**Question 1**

Alternatively:

- a. Recognize that  $\mathbf{x} \cdot \mathbf{A} \cdot \mathbf{x} = \mathbf{A} : (\mathbf{x} \otimes \mathbf{x})$ , with  $\mathbf{x} \otimes \mathbf{x}$  a symmetric second-order tensor; followed by recalling that the scalar product of a symmetric and a skewsymmetric tensor vanishes. 1

1

- b. Introduce symmetric and skew-symmetric parts  $\mathbf{S}$  and  $\mathbf{W}$ , respectively, and expand:

$$\mathbf{x} \cdot \mathbf{A} \cdot \mathbf{x} = \mathbf{x} \cdot \mathbf{S} \cdot \mathbf{x} + \mathbf{x} \cdot \mathbf{W} \cdot \mathbf{x};$$

exploit the skewsymmetry of  $\mathbf{W}$  to derive 1

1

$$\mathbf{x} \cdot \mathbf{W} \cdot \mathbf{x} = x_i W_{ij} x_j = -x_i W_{ji} x_j = -x_j W_{ij} x_i = -x_i W_{ij} x_j = -\mathbf{x} \cdot \mathbf{W} \cdot \mathbf{x} = 0.$$

1

**Question 2**

- a. Since  $F_{ij} = \delta_{ij} + u_{i,j}$ , the only-nonzero component of the displacement gradient is  $u_{2,1} = \gamma$ . Substitution into  $\epsilon_{ij} = \frac{1}{2}(u_{i,j} + u_{j,i})$  yields the specified strain components. 1

1

- b. No, the inverse is not correct, since there are many displacement gradients that satisfy  $\frac{1}{2}(u_{1,2} + u_{2,1}) = \gamma/2$ . More specifically, there are many rotations  $\omega_{ij} = \frac{1}{2}(u_{i,j} - u_{j,i})$  that can be added to the given state of strain  $\epsilon_{ij}$  in order to arrive at the displacement gradient. The one given in the question corresponds to a particular rotation:  $\omega_{12} = -\gamma/2$ . 2

2

**Question 3**

It is the traction across the interface that needs to be continuous, as a consequence of Newton's third law (action = -reaction). Since 1

1

$$\mathbf{t} = \boldsymbol{\sigma} \cdot \mathbf{n} = \sigma_{i2} \mathbf{e}_i,$$

the components  $\{\sigma_{12}, \sigma_{22}, \sigma_{23}\}$  are continuous (note that the normal stresses parallel to the interface, i.e.  $\sigma_{11}$  and  $\sigma_{33}$  can change discontinuously) 1

1

**Question 4**

This question is most easily answered with reference to the elementary Mohr's circle, but also through the transformation formulas.

- a. When  $2\theta = 90^\circ$ , hence  $\theta = 45^\circ$ . 1

1

- b.  $\frac{1}{2}(\epsilon_1 + \epsilon_2)$  1

1